

SCS ENGINEERS

Environmental Consultants & Contractors
15521 Midlothian Turnpike
Suite 305
Midlothian, VA 23113-7313
804 378-7440 FAX 804 378-7433
www.scsengineers.com

JOB NO. 02218208.17 - Bristol SWP 498
SHEET NO. 1 OF 1
CALCULATED BY TRW DATE 2/10/2023
CHECKED BY CJW DATE 2/17/2023
SUBJECT IV - ESTIMATED MAXIMUM SETTLEMENT

Purpose:

Estimate the maximum amount of settlement of the final cover system that may occur.

Given:

Based upon assumed base grades for the SWP #498 landfill provided by others and the design final closure grade, the maximum depth of waste may be estimated as:

Maximum Waste Depth ≈ **50** ft

Based upon historical experience and research, SCS estimates the long-term waste settlement as **10%** of the original depth. SCS believes this estimate to be conservative due to the age of the waste and the previous landfill mining activities at the site.

Approximate Waste Settlement ≈ **10** %

Calculation

$Estimated\ Settlement = Waste\ Depth \times Settlement\ \% = 50ft \times 10\% = 5\ ft$

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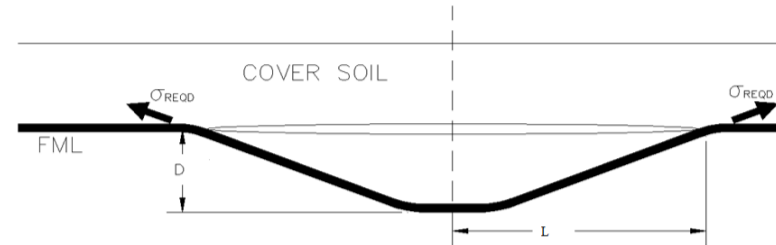
JOB NO. 02218208.17 - Bristol SWP 498
 SHEET NO. 1 OF 1
 CALCULATED BY TRW DATE 2/10/2023
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 SUBJECT IV - LLDPE STRESS DUE TO SUBSIDENCE

Purpose:

Determine the stress in the final cover geomembrane (40 mil textured LLDPE) due to potential severe (approx. worse case) differential settlement and compare with the geomembrane break strength.

Given:

The required strength (σ_{reqd}) of the geomembrane may be calculated as:



$$\sigma_{reqd} = \frac{2DL^2\gamma_{CS}H_{CS}}{3t(D^2 + L^2)}$$

Reference: Design and Construction of RCRA-CERCLA Final Covers
 United States Environmental Protection Agency
 Office of Research and Development, May 1991

where:

- | | | | |
|---------------|-----------------------------|---|--------------------------------------|
| D | = differential settlement | = | assumed 5 foot, see figure |
| L | = radius of settlement area | = | assumed 10 feet, see figure |
| t | = thickness of geomembrane | = | 40 mil, see technical specifications |
| H_{CS} | = height of cover soil | = | 2 feet, see final cover details |
| γ_{CS} | = unit weight of cover soil | = | assumed 110 pcf |

The 40 mil LLDPE geomembrane break strength is specified as 60 lb/in (1500 psi) by the technical specifications.

Calculation

$$\sigma_{reqd} = \frac{2DL^2\gamma_{CS}H_{CS}}{3t(D^2+L^2)} = \frac{2(5ft)(10ft)^2(110pcf)(2ft)}{3(\frac{0.40}{12}ft)((5ft)^2+(10ft)^2)} = 176,000 \text{ lb/ft}^2 = 1222 \text{ lb/in}^2$$

1222 lb/in² is required to resist the stress from assumed differential settlement

The factor of safety is given by:

$$FS = \frac{\sigma_{break\ strength}}{\sigma_{reqd}} = \frac{1500 \text{ psi}}{1222 \text{ psi}} = 1.23 \text{ OK}$$